



Accuracy of Interchangeable Implant Impression Systems: An In Vitro Pilot Study

AU2

Abdullah M. AlFarraj Aldosari, BDS, DMSc,* Abdulaziz M. AlBaker, BDS, MS,† Abdulmonem A. AlShihri, BDS,‡ Majid I. AlJadeed, BDS,§ Loay A. AlBwardi, BDS,|| and Sukumaran Anil, BDS, MDS, PhD, FDSRCPS (Glas)¶

The introduction of the original implant system (Brånemark) was followed by several alternative systems (implant and components) closely resembling the original design and treatment protocol.¹⁻⁶ Fixation screws, laboratory components, and tools can be used interchangeably between Brånemark and BIOMET 3i and between Straumann and Allfit implant systems.⁷

Patients may present with implants already placed in the maxillae or mandible. This situation often presents serious problems because the restorative dentist may not know which type of implant was placed, unless he/she has access to the patient records. Incidents have been anecdotally cited in which different types of implants have been placed in the same mouth or even in the same arch. Therefore, in such cases, the availability of different

Purpose: To evaluate the accuracy of impressions on changing the implant component (coping and abutment replica) between Brånemark and BIOMET 3i and between Straumann and Allfit.

Materials and Methods: Two master casts were constructed, one containing pair of Brånemark self-tap Mk II fixtures (Nobel Biocare) labeled Master cast I and the other containing pair of Straumann Standard plus implant, SLA fixtures (Straumann) labeled Master cast II. Ten impressions of each master cast were made by open tray technique using polyether impression material. Five out of 10 impressions made from master cast I contained Brånemark pair of coping and replica and the other 5 contained 3i (Implant Innovations). Five out of

10 impressions made from master cast II contained Straumann pair of copings and replica and the remaining 5 contained Allfit implants (Ihde Dental). Duplicated casts were prepared, and distances between copings were measured using traveling microscope and compared the distance in master casts.

Result: No significant difference was observed in mean value between 2 master casts and their duplicates.

Conclusion: The interchangeability of coping and abutment replica between Brånemark and BIOMET 3i and between Straumann and Allfit was found to be possible without compromising the quality of impressions. (Implant Dent 2015;24:1-6)

Key Words: dental implant systems, impression accuracy, interchangeability, transfer coping

*Associate Professor and Consultant of Prosthodontics and Implantology; Director of Dental Implant and Osseointegration Research Chair, College of Dentistry, King Saud University, Riyadh, Saudi Arabia.

†Associate Professor, Department of Prosthetic Dental Sciences, College of Dentistry, King Saud University, Riyadh, Saudi Arabia.

‡Postgraduate Student, Harvard School of Dental Medicine, Boston, MA.

§Resident, Riyadh Military Hospital, Riyadh, Saudi Arabia.

||Resident, Ministry of Health, Riyadh, Saudi Arabia.

¶Professor, Department of Periodontics and Community Dentistry, College of Dentistry, King Saud University, Riyadh, Saudi Arabia.

Reprint requests and correspondence to: Abdullah M. AlFarraj Aldosari, BDS, DMSc, College of Dentistry, King Saud University, Riyadh 11545, Saudi Arabia, Phone: +966 505807202, Fax: +966 4678548.

ISSN 1056-6163/15/02402-001

Implant Dentistry

Volume 24 • Number 2

Copyright © 2015 Wolters Kluwer Health, Inc. All rights reserved.

DOI: 10.1097/ID.0000000000000231

implant components would be beneficial for the patient.

Lang et al⁸ evaluated the fitness of precision between the Procera (Nobel Biocare Management AG, Zürich-Flughafen, Switzerland) custom abutment and various implant systems and found that the Procera abutment fits into the internal threading of the entire external hexagon implants studied. Jaarda et al⁹ studied the geometry of 5 interchangeable prosthetic retaining screws (3i Implant Innovation-gold, Impla-Med-gold, Nobelpharma-gold, 3i Implant Innovation-

titanium, and Implant Support Systems-titanium). They found significant differences between screws and concluded that interchanging prosthetic retaining screws might introduce unknown variables when treating patients. They also reported that the ultimate tensile strength of the 5 interchangeable prosthetic retaining screws were significantly different from the control screws, thereby suggesting that interchanging prosthetic retaining screws will influence their accuracy feature.¹⁰

In a review of studies referring to success and failure in osseointegrated

AU3

AU4

AU1

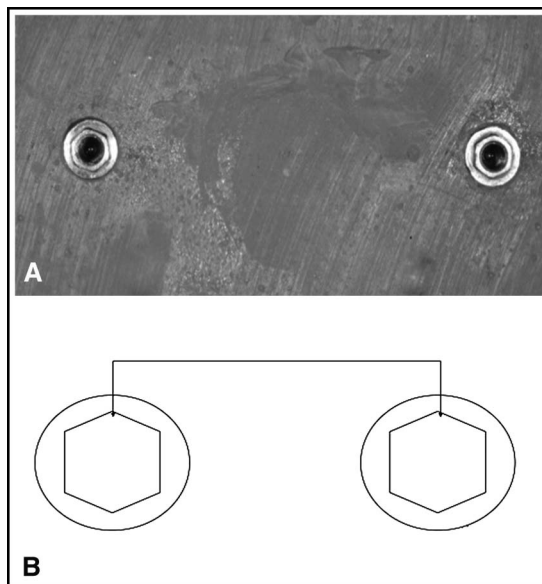


Fig. 1. **A**, Block, which contains a pair of Brånemark fixture (master cast I). **B**, The fixed points in the hexa that were used for measurement.

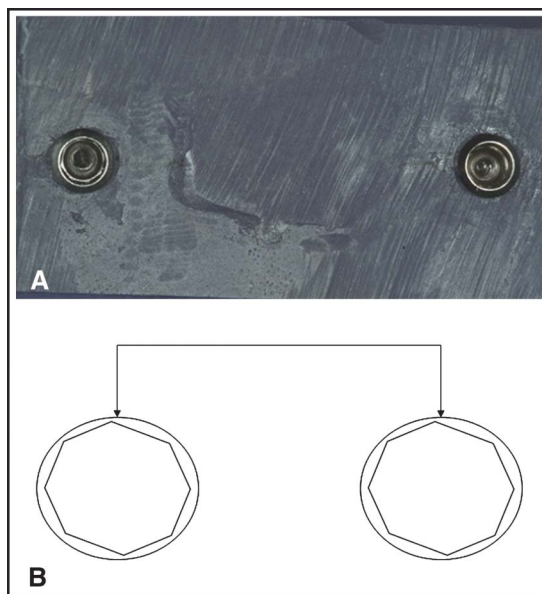


Fig. 2. **A**, Block, which contains a pair of Straumann fixture (master cast II). **B**, The fixed points in the octa that were used for measurement.

implant treatment published between 1981 and 1997, Goodacre et al¹¹ studied the mechanical and biological problems associated with dental implant treatment. The authors mentioned prostheses and abutment screw loosening, implant fracture and fracture of the metal framework, and the restorative material used as some of the mechanical problems associated with dental implant treatment. Misfit of components was cited

as a possible cause of these complications. Although the causes for the failure of a prosthesis are multifactorial, it must be assumed that prosthesis misfit plays an important role in complications, such as screw loosening, screw fractures, plaque retention, etc.^{12–16}

Therefore, care must be taken to minimize prosthesis misfit. There has been no clear consensus on the effect of interchanging the impression

coping and replica between comparable implant systems on the accuracy of the impressions made.^{17,18} Currently, there is no literature available on the use of alternative coping and abutment replica systems. The studies on interchangeability of abutments have showed inaccuracy at the implant-abutment interface. It was also noted that the potential for significant precision problems may be even greater than expected when all the elements are furnished by the same manufacturer.^{17,19}

Hence, the aim of this *in vitro* pilot study was to evaluate the accuracy of impressions on changing the implant component (coping and abutment replica) between Brånemark and 3i and between Straumann and Allfit.

MATERIALS AND METHODS

Two master casts were constructed. The first master cast contained a pair of 4×15 mm Brånemark self-tap Mk II fixtures (Nobel Biocare AB, Gothenburg, Sweden), and this master cast was assigned as “Master cast I.” The second master cast contained a pair of 4.1×12 mm Straumann Standard plus implant, SLA fixtures (Straumann Institute, Waldenburg, Switzerland) and was assigned as “Master cast II.”

Ten impressions of each master cast were made by open tray technique using a polyether impression material. Five out of the 10 impressions made from master cast I contained Brånemark pair of coping and replica, and the other 5 contained 3i (Implant Innovations Inc, West Palm Gardens, FL). Five out of the 10 impressions made from master cast II contained Straumann pair of copings and replica, and the remaining 5 contained Allfit implants (Ihde Dental AG, Switzerland) (Table 1).

AU5
T1

Master Cast Model Design

Two blocks were constructed from chemical-cured ortho resin (Orthoresin; Dentsply, DeguDent GmbH, Postfach, Hanau, Germany). The material was mixed and then poured in customized flasks that had been previously fabricated. The material was allowed to set according to the manufacturer's instructions. After the setting, the blocks were taken out of the flasks and trimmed off the excess. Then, 2 points

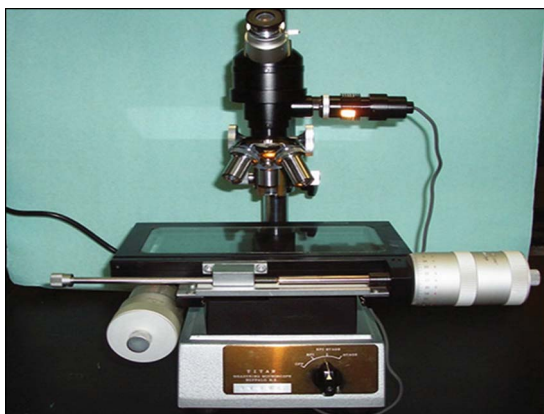


Fig. 3. Traveling microscope used for the measurement of distance between reference points.

were marked on each block with a specific distance. Two holes were made using a straight handpiece with a fissure bur at the marked points.

Two Brånemark fixtures (Nobel Biocare AB) and 2 Straumann fixtures (Straumann Institute, Waldenburg, Switzerland) were inserted and relined individually into the prepared holes. A Ney surveyor was used to confirm an exact path of insertion of the 2 fixtures. Master cast I contained 2 Brånemark fixtures (Fig. 1, A), and master cast II contained 2 Straumann fixtures (Fig. 2, A). Two reference points were selected, which represented the head of the helix in Brånemark system (Fig. 1, B) and the head of the octa of the Straumann system (Fig. 2, B). Measurements were taken using a traveling microscope (Titan, Buffalo, NY). Three readings were taken for each master model, and the average of the 3 readings were used as reference distance to which the

distances on the duplicated models were compared.

Impression Tray Design

Impressions were made with an open tray technique using a custom tray. Copings were screwed into the fixtures using their specific screws. To standardize the torque at 10 N·cm, a calibrated torque controller was used. One layer of wax spacer was applied, covering the superior surface of the master cast without covering the coping and the cast stoppers. Then, 2 layers of wax spacer were wrapped around the copings. Chemically cured polymethyl

methacrylate acrylic resin (Fastray; Harry J. Bosworth Company, Skokie, IL) was mixed and adapted over the wax spacer, and then the material was allowed to set according to the manufacturer's instructions. Holes were made over the copings (using a straight handpiece with a fissure bur), and the thickness of the flanges was reduced from the inner surface to allow the excess impression material to escape during the impression making. Ten custom trays were duplicated from each master cast. The duplication was made by using the silicon impression material in prefabricated flasks.

Impression Protocol

Twenty impressions were made using polyether (Impregum Penta Soft; 3M ESPE) to transfer the copings from the fixture to the cast. Ten impressions were made from the first master cast (Brånemark system) out of which 5 impressions transferred Brånemark coping and replica (Nobel Biocare) and the other 5 transferred the interchangeable 3i coping and replica (Implant Innovation).

Similarly, for the second master cast (Straumann system), 5 impressions transferred Straumann coping and replica and the other 5 transferred the interchangeable Allfit coping and replica (BioMed Est; Ihde Dental AG). The impressions were made using a Pentamix mixing machine (Pentamix 2; 3M ESPE) to have a uniform mixing. The trays were loaded with impression material and allowed to set according to the manufacturer's instructions. Transfer copings were unscrewed and connected to abutment replica.

Cast Production Protocol

The impressions were poured with Royal boxing wax wrapped around each tray. The mix was prepared with dental stone (GC Fujirock EP, Japan) using a vacuum-mixing machine, and then poured using a vibrating machine (Vibromaster; Bego Bremer Goldshagerel will GmBA & Co., Bremen, Germany). The material was allowed to set according to the manufacturer's instructions. Then, the blocks were trimmed to refine the shape of the blocks.

F1

F2

Table 1. The Distance Between the Reference Points on Master Model 1 (Brånemark Fixtures, 30.011 mm) and Experimental Models (Brånemark and 3i Fixtures)

Model No.	Brånemark	3i
1	30.038	29.899
2	29.969	30.123
3	30.029	29.989
4	29.989	29.994
5	30.101	29.389
Mean	30.025	29.879
SD	0.051	0.285

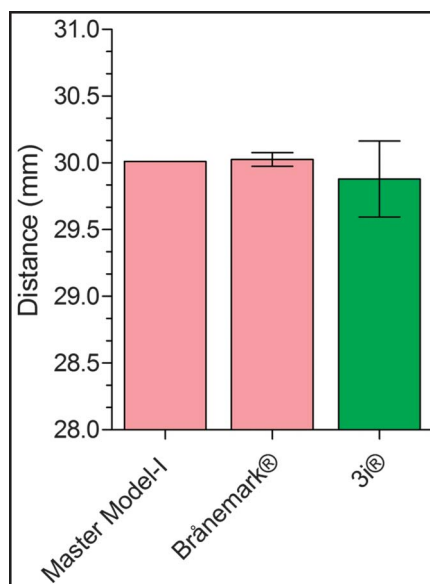


Fig. 4. Variation in distance between the reference points on Master model I (Brånemark fixtures) and experimental models.

Table 2. The Distance Between the Reference Points on Master Model 2 (Straumann Fixtures, 30.011 mm) and Experimental Models (Straumann and Allfit Fixtures)

Model No.	Straumann	Allfit
1	30.239	30.219
2	30.211	29.453
3	30.099	29.717
4	30.175	30.119
5	30.012	29.579
Mean	30.147	29.817
SD	0.092	0.336

Measurement Protocol

A traveling microscope (Titan) (Fig. 3) was used to measure the distance between the 2 reference points that were determined in the master cast. The measurements were taken by fixing the casts on the microscope, which allowed a controlled movement of the casts. Reference point for the measurements was fixed for each of the implant systems. The head of the hex in external hex implant system (Brånemark and 3i) and the head of the octa in the internal octa implant system (Straumann and Allfit) were used as the reference points. The values obtained for the master model I and II were then compared to the duplicated models. Three readings were taken for each duplicated cast. The average distance of the 3 readings were taken and compared with that of the master cast.

All statistical analysis was performed using One-Sample *t* test in SPSS program (version 10), and descriptive data analysis was used to report findings.

RESULTS

The distance between the reference points is depicted in Tables 1 and 2. Both master Model I and II measured a distance of 30.011 mm. The dimensions for Master model I (Brånemark) and its duplicated models and 3i models are shown in Table 1 and Figure 4. The mean distance for Brånemark duplicated models was 30.025 ± 0.051 and 29.879 ± 0.285 for the 3i models. Although, the Brånemark duplicated models showed more accuracy, both systems were statistically not significant from the master model ($P > 0.05$).

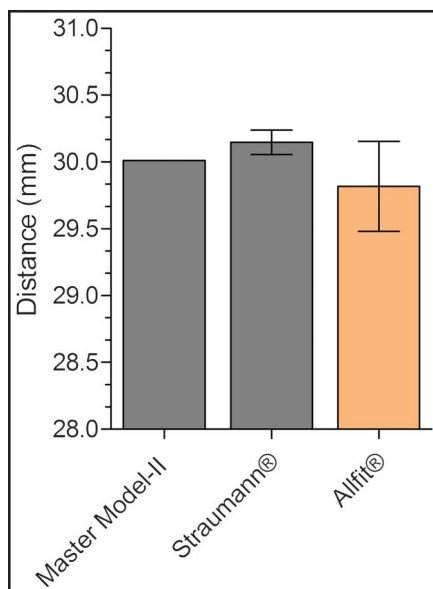


Fig. 5. Variation in distance between Master model I (ITI fixtures) and experimental models.

Table 2 and Figure 5 present the distance between the reference points on the master model II and its duplicated Straumann and Allfit models. The Straumann models showed a mean distance of 30.147 ± 0.092 . The mean distance for the Allfit duplicated models was 29.817 ± 0.336 . Comparison of the distance with the master cast did not reveal any statistical significance ($P > 0.05$).

DISCUSSION

The success of implant treatment results from biologic and mechanical factors.²⁰ A critical element in implant prosthodontics is to fabricate a supra-structure that fits accurately to the implants to avoid the increased risk of technical and biological complications.^{21–23} An acceptable prosthesis requires optimal accuracy in all steps of fabrication. The implant-abutment joint, maintained by a retention force generated by the screw, is an essential biomechanical factor that withstands occlusal forces.²⁴

The precision of the prosthesis depends on the accuracy of positioning the impression components and recording the implant position with the impression procedure.^{7,25} The impression can be made either at the abutment

level using a transfer coping and a pickup impression technique with the coping retained in the impression while it is removed from the mouth or at the implant level using 2 methods: the pickup method or the repositioning method, in which a tapered impression coping is retained on the implant and later removed from the mouth, reassembled with the implant analog, and replaced tightly into the impression.^{26,27}

Clinical situations demand for brand switching and/or use of universal components in implant dentistry. Studies showed that the potential for precision problems were greater when all the elements are furnished by the same manufacturer.¹⁷ In this study, we found that there was no significant difference in the accuracy of the impression and models by interchanging the coping and replica among the various implant systems studied. This observation is in agreement with similar studies, which attempted to change the abutments and screws.^{17,28}

Precious metal alloys are preferred over base metals in implant restorations to avoid the potential for corrosion between dissimilar metals. It is assumed that corrosion of precious metals against titanium would likely be less than that seen with base metals, and by-products of the corrosion process would be less likely to be toxic or allergenic than their base metal counterparts.²⁹

The use of fixture-level impression technique was expected to record only the implant head position rather than both its position and dimensions. Both of these factors would suggest that the impression distortion was likely to have less effect as compared with the conventional fixed prosthodontic impressions.³⁰ Also, impression accuracy was increased by using custom trays because it has been shown that a difference in the thickness of elastomeric impression material in an impression tray could reduce its accuracy.^{31,32} Another point of importance aimed at maximizing the accuracy of transferring the fixture and abutment/coping relation was the use of polyether impression material that has good dimensional stability and accuracy.^{18,33}

The implant impression using impression copings requires a connection

to the implant or the abutment. After separating the impression, another connection between the impression coping and an implant analog is required to fabricate a definitive cast. Because the connection between 2 metal components may occur with various spatial relations at the micrometer level, the implant impression has an inherent discrepancy. This is considered as “machining tolerance” and reported that the measured tolerances ranged from 22 μm to 100 μm .³⁴ Hence, while interpreting the studies investigating the implant impression accuracy, the machining tolerance should be considered as one of factors affecting accuracy.¹⁸ Hence, in this study also, we found negligible discrepancy when the impression coping of the same system or a similar system is used. In a systematic review, a linear discrepancy of 0.6 μm to 136 μm between the definitive cast and experimental model was considered as a consequence of machining tolerance.¹⁸ The impression coping with different designs showed a different level of impression accuracy, and to increase the accuracy, the coping was extended or treated with airborne-particle abrasion and impression adhesive.^{27,35}

Although our findings present no statistically significant differences in interchanged components, the observations clearly reinforce the advantages of using the same implant components. In general, based on the findings, it is recommended that the components of the same system be used for routine procedures. However, the use of components from alternative system can also be considered because it does not affect the accuracy.^{12,18}

CONCLUSION

Within the limitation of this study, the Brånemark and Straumann master models, reference points on BIOMET 3i and Allfit duplicated models showed values with no statistically significant difference. Although it is desirable to use components such as coping and abutment replica from same system, the accuracy is not compromised by using components from identical systems. Because this study is done in an *in vitro* setup, it may be considered as a limitation.

DISCLOSURE

The authors claim to have no financial interest, either directly or indirectly, in the products or information listed in the article.

ACKNOWLEDGMENTS

The authors wish to acknowledge the support provided by the Dental Implant and Osseointegration Research Chair, King Saudi University, Riyadh, Saudi Arabia.

REFERENCES

- Binon PP. Evaluation of three slip fit hexagonal implants. *Implant Dent*. 1996;5:235–248.
- Tsuge T, Hagiwara Y, Matsumura H. Marginal fit and microgaps of implant-abutment interface with internal anti-rotation configuration. *Dent Mater J*. 2008;27:29–34.
- Binon PP, McHugh MJ. The effect of eliminating implant/abutment rotational misfit on screw joint stability. *Int J Prosthodont*. 1996;9:511–519.
- Binon PP. Evaluation of machining accuracy and consistency of selected implants, standard abutments, and laboratory analogs. *Int J Prosthodont*. 1995;8:162–178.
- Byrne D, Houston F, Cleary R, et al. The fit of cast and premachined implant abutments. *J Prosthet Dent*. 1998;80:184–192.
- Jansen VK, Conrads G, Richter EJ. Microbial leakage and marginal fit of the implant-abutment interface. *Int J Oral Maxillofac Implants*. 1997;12:527–540.
- Dellow AG, Driessen CH, Nel HJ. Scanning electron microscopy evaluation of the interfacial fit of interchanged components of four dental implant systems. *Int J Prosthodont*. 1997;10:216–221.
- Lang LA, Sierraalta M, Hoffensperger M, et al. Evaluation of the precision of fit between the Procera custom abutment and various implant systems. *Int J Oral Maxillofac Implants*. 2003;18:652–658.
- Jaarda MJ, Razzoog ME, Gratton DG. Geometric comparison of five interchangeable implant prosthetic retaining screws. *J Prosthet Dent*. 1995;74:373–379.
- Jaarda MJ, Razzoog ME, Gratton DG. Ultimate tensile strength of five interchangeable prosthetic retaining screws. *Implant Dent*. 1996;5:16–19.
- Goodacre CJ, Kan JY, Rungcharassaeng K. Clinical complications

of osseointegrated implants. *J Prosthet Dent*. 1999;81:537–552.

12. Barbosa GA, Bernardes SR, das Neves FD, et al. Relation between implant/abutment vertical misfit and torque loss of abutment screws. *Braz Dent J*. 2008;19:358–363.

13. Kallus T, Bessing C. Loose gold screws frequently occur in full-arch fixed prostheses supported by osseointegrated implants after 5 years. *Int J Oral Maxillofac Implants*. 1994;9:169–178.

14. Hebel KS, Gajjar RC. Cement-retained versus screw-retained implant restorations: Achieving optimal occlusion and esthetics in implant dentistry. *J Prosthet Dent*. 1997;77:28–35.

15. Watanabe F, Uno I, Hata Y, et al. Analysis of stress distribution in a screw-retained implant prosthesis. *Int J Oral Maxillofac Implants*. 2000;15:209–218.

16. Goodacre CJ, Bernal G, Rungcharassaeng K, et al. Clinical complications with implants and implant prostheses. *J Prosthet Dent*. 2003;90:121–132.

17. Zanardi PR, Costa B, Stegun RC, et al. Connecting accuracy of interchanged prosthetic abutments to different dental implants using scanning electron microscopy. *Braz Dent J*. 2012;23:502–507.

18. Lee H, So JS, Hochstedler JL, et al. The accuracy of implant impressions: A systematic review. *J Prosthet Dent*. 2008;100:285–291.

19. Emekli C, Odman P, Ortengren U, et al. An *in vitro* load evaluation of a conical implant system with 2 abutment designs and 3 different retaining-screw alloys. *Int J Oral Maxillofac Implants*. 2006;21:733–737.

20. Kitamura E, Stegaroiu R, Nomura S, et al. Biomechanical aspects of marginal bone resorption around osseointegrated implants: Considerations based on a three-dimensional finite element analysis. *Clin Oral Implants Res*. 2004;15:401–412.

21. Brunski JB. *In vivo* bone response to biomechanical loading at the bone/dental-implant interface. *Adv Dent Res*. 1999;13:99–119.

22. Sahin S, Cehreli MC. The significance of passive framework fit in implant prosthodontics: Current status. *Implant Dent*. 2001;10:85–92.

23. Bayraktar M, Gultekin BA, Yalcin S, et al. Effect of crown to implant ratio and implant dimensions on peri implant stress of splinted implant-supported crowns: A finite element analysis. *Implant Dent*. 2013;22:406–413.

24. Sahin S, Cehreli MC, Yalcin E. The influence of functional forces on the biomechanics of implant-supported prostheses—A review. *J Dent*. 2002;30:271–282.

25. Stuker RA, Teixeira ER, Beck JC, et al. Preload and torque removal evaluation of three different abutment screws for single standing implant restorations. *J Appl Oral Sci.* 2008;16:55–58.
26. Daoudi MF, Setchell DJ, Searson LJ. A laboratory investigation of the accuracy of two impression techniques for single-tooth implants. *Int J Prosthodont.* 2001;14:152–158.
27. Herbst D, Nel JC, Driessen CH, et al. Evaluation of impression accuracy for osseointegrated implant supported superstructures. *J Prosthet Dent.* 2000;83:555–561.
28. Hsu CC, Millstein PL, Stein RS. A comparative analysis of the accuracy of implant transfer techniques. *J Prosthet Dent.* 1993;69:588–593.
29. Lygre H. Prosthodontic biomaterials and adverse reactions: A critical review of the clinical and research literature. *Acta Odontol Scand.* 2002;60:1–9.
30. Burns J, Palmer R, Howe L, et al. Accuracy of open tray implant impressions: An in vitro comparison of stock versus custom trays. *J Prosthet Dent.* 2003;89:250–255.
31. Boulton JL, Gage JP, Vincent PF, et al. A laboratory study of dimensional changes for three elastomeric impression materials using custom and stock trays. *Aust Dent J.* 1996;41:398–404.
32. Cehreli MC, Akca K. Impression techniques and misfit-induced strains on implant-supported superstructures: An in vitro study. *Int J Periodontics Restorative Dent.* 2006;26:379–385.
33. Chee W, Jivraj S. Impression techniques for implant dentistry. *Br Dent J.* 2006;201:429–432.
34. Ma T, Nicholls JI, Rubenstein JE. Tolerance measurements of various implant components. *Int J Oral Maxillofac Implants.* 1997;12:371–375.
35. Vigolo P, Majzoub Z, Cordioli G. In vitro comparison of master cast accuracy for single-tooth implant replacement. *J Prosthet Dent.* 2000;83:562–566.