

EE310

Solved Problems on MOSFETs

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4.3 With the knowledge that $\mu_p \approx 0.4\mu_n$, what must be the relative width of n -channel and p -channel devices if they are to have equal drain currents when operated in the saturation mode with overdrive voltages of the same magnitude?

$$I_{D-n} = I_{D-p}$$

$$\frac{k'_n}{2} \times \frac{W_n}{L} \times (V_{ov})^2 = \frac{k'_p}{2} \times \frac{W_p}{L} \times (V_{ov})^2$$

$$k'_n \times W_n = k'_p \times W_p, \text{ but } k'_n = \mu_n \times C_{ox} \text{ and } k'_p = \mu_p \times C_{ox}$$

$$\Rightarrow \mu_n \times C_{ox} \times W_n = \mu_p \times C_{ox} \times W_p,$$

$$\text{or } \mu_n \times W_n = \mu_p \times W_p \Rightarrow \frac{W_p}{W_n} = \frac{\mu_n}{\mu_p} = \frac{\cancel{\mu_n}}{0.4 \cancel{\mu_n}} = 2.5$$

4.4 An n -channel device has $k'_n = 50 \mu\text{A}/\text{V}^2$, $V_t = 0.8 \text{ V}$, and $W/L = 20$. The device is to operate as a switch for small v_{DS} , utilizing a control voltage v_{GS} in the range 0 V to 5 V. Find the switch closure resistance, r_{DS} , and closure voltage, V_{DS} , obtained when $v_{GS} = 5 \text{ V}$ and $i_D = 1 \text{ mA}$. Recalling that $\mu_p \approx 0.4\mu_n$, what must W/L be for a p -channel device that provides the same performance as the n -channel device in this application?

$$r_{DS} = \frac{1}{k'_n \times \left(\frac{W_n}{L_n}\right) \times V_{ov}} = \frac{1}{k'_n \times \left(\frac{W_n}{L_n}\right) \times (V_{GS} - V_t)} = \frac{1}{50 \times 10^{-6} \times (20) \times (5 - 0.8)} = 238 \Omega$$

$$v_{DS} = i_D \times r_{DS} = 1 \times 10^{-3} \times 238 = 238 \text{ mV}$$

$$\frac{W_p}{L_p} = 2.5 \frac{W_n}{L_n} = 50$$

4.5 An n -channel MOS device in a technology for which oxide thickness is 20 nm, minimum gate length is 1 μm , $k'_n = 100 \mu\text{A}/\text{V}^2$, and $V_t = 0.8 \text{ V}$ operates in the triode region, with small v_{DS} and with the gate-source voltage in the range 0 V to +5 V. What device width is needed to ensure that the minimum available resistance is 1 k Ω ? W_{max}

$$r_{DS} = \frac{1}{k'_n \times \left(\frac{W_n}{L_n}\right) \times V_{OV}} = \frac{1}{k'_n \times \left(\frac{W_n}{L_n}\right) \times (V_{GS} - V_t)}$$

for $V_{GS} > V_t$ and very close to V_t , r_{DS} will be very large \Rightarrow no worries!

for $V_{GS} = 5$, there is a risk that r_{DS} will fall below 1 k Ω .

$$\frac{1}{k'_n \times \left(\frac{W_n}{L_n}\right) \times (V_{GS} - V_t)} \geq 1 \text{ k}\Omega \Rightarrow \frac{1}{100 \times 10^{-6} \times \left(\frac{W_n}{1 \times 10^{-6}}\right) \times (5 - 0.8)} \geq 1000$$

$$420000 \times W_n \leq 1 \Rightarrow W_n \leq 2.38 \mu\text{m}$$

4.6 Consider a CMOS process for which $L_{\min} = 0.8 \mu\text{m}$, $t_{ox} = 15 \text{ nm}$, $\mu_n = 550 \text{ cm}^2/\text{V} \cdot \text{s}$, and $V_t = 0.7 \text{ V}$.

(a) Find C_{ox} and k'_n .

(b) For an NMOS transistor with $W/L = 16 \mu\text{m}/0.8 \mu\text{m}$, calculate the values of V_{OV} , V_{GS} , and $V_{DS\min}$ needed to operate the transistor in the saturation region with a dc current $I_D = 100 \mu\text{A}$.

(c) For the device in (b), find the value of V_{OV} and V_{GS} required to cause the device to operate as a 1000- Ω resistor for very small v_{DS} .

a)

$$C_{ox} = \frac{\epsilon_{r(ox)} \times \epsilon_o}{t_{ox}} = \frac{3.9 \times 8.854 \times 10^{-12}}{15 \times 10^{-9}} = 2.3 \times 10^{-3} \text{ F/m}^2 = 2.3 \times 10^{-7} \text{ F/cm}^2$$

$$k'_n = \mu_n \times C_{ox} = 550 \times 2.3 \times 10^{-7} = 1.265 \times 10^{-4} \text{ A/V}^2 = 126.5 \text{ } \mu\text{A/V}^2$$

b)

$$i_D = \frac{k'_n}{2} \times \left(\frac{W}{L}\right) \times (v_{GS} - V_t)^2, i_D = \frac{k'_n}{2} \times \left(\frac{W}{L}\right) \times (V_{OV})^2 \Rightarrow 100 = \left(\frac{126.5}{2}\right) \times \left(\frac{16}{0.8}\right) \times (V_{OV})^2$$

$$\Rightarrow (V_{OV})^2 = 0.07905 \Rightarrow V_{OV} = \pm 0.2812 \text{ V, select } V_{OV} = + 0.2812 \text{ V}$$

$$V_{OV} = V_{GS} - V_t \text{ (for NMOS)} \Rightarrow V_{GS} = V_{OV} + V_t = 0.2812 + 0.7 = 0.9812 \text{ V}$$

$$V_{DS(\min)} = V_{DS(\text{sat})} = V_{OV}$$

c)

$$r_{DS} = \frac{1}{k'_n \times \left(\frac{W_n}{L_n}\right) \times V_{OV}} \Rightarrow 1000 = \frac{1}{126.5 \times 10^{-6} \times \left(\frac{16}{0.8}\right) \times V_{OV}} \Rightarrow V_{OV} = 0.3953 \text{ V}$$

$$V_{GS} = V_{OV} + V_t = 0.3953 + 0.7 = 1.0953 \text{ V}$$

4.19 For a particular MOSFET operating in the saturation region at a constant v_{GS} , i_D is found to be 2 mA for $v_{DS} = 4 \text{ V}$ and 2.2 mA for $v_{DS} = 8 \text{ V}$. What values of r_o , V_A , and λ correspond?

4.20 A particular MOSFET has $V_A = 50 \text{ V}$. For operation at 0.1 mA and 1 mA, what are the expected output resistances? In each case, for a change in v_{DS} of 1 V, what percentage change in drain current would you expect?

{4.19}

$I_{D1} = 2 \text{ mA @ } V_{DS1} = 4 \text{ V}$ $I_{D2} = 2.2 \text{ mA @ } V_{DS2} = 8 \text{ V}$	V_{GS} is constant; Find r_o , λ , and V_A .
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$$r_o = \frac{\Delta V_{DS}}{\Delta I_D} = \frac{(8 - 4)}{(2.2 - 2) \times 10^{-3}} = 20 \text{ k}\Omega$$

$$\frac{I_{D1}}{I_{D2}} = \frac{\frac{k'_n}{2} \times \frac{W}{L} \times (V_{GS} - V_t)^2 \times (1 + \lambda V_{DS1})}{\frac{k'_n}{2} \times \frac{W}{L} \times (V_{GS} - V_t)^2 \times (1 + \lambda V_{DS2})} \Rightarrow \frac{I_{D1}}{I_{D2}} = \frac{(1 + \lambda V_{DS1})}{(1 + \lambda V_{DS2})} \Rightarrow (1 + \lambda V_{DS2}) I_{D1} = (1 + \lambda V_{DS1}) I_{D2} \Rightarrow$$

$$\lambda = \frac{I_{D2} - I_{D1}}{V_{DS2} \times I_{D1} - V_{DS1} \times I_{D2}} = 0.0278 \text{ V}^{-1} \rightarrow V_A = \frac{1}{\lambda} = 36 \text{ V}$$

{4.20}

$$@ I_D = 0.1 \text{ mA}, r_o = \frac{V_A}{I_D} = \frac{50}{0.1 \times 10^{-3}} = 500 \text{ k}\Omega \quad @ I_D = 1 \text{ mA}, r_o = \frac{V_A}{I_D} = \frac{50}{1 \times 10^{-3}} = 50 \text{ k}\Omega$$

$$r_o = \frac{\Delta V_{DS}}{\Delta I_D}, \Rightarrow \Delta I_D = \frac{\Delta V_{DS}}{r_o} = \frac{1}{500 \times 10^3},$$

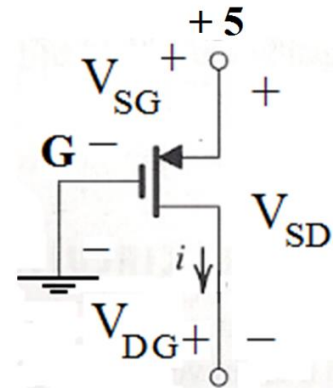
For the $I_D = 0.1 \text{ mA}$ case,

$$\left(\frac{\Delta I_D}{I_D} \right) \times 100 = \left[\left(\frac{1}{500 \times 10^3} \right) \div 0.1 \times 10^{-3} \right] \times 100 = 2\%$$

For the $I_D = 1 \text{ mA}$ case,

$$\Delta I_D = \frac{\Delta V_{DS}}{r_o} = \frac{1}{50 \times 10^3}, \left(\frac{\Delta I_D}{I_D} \right) \times 100 = \left[\left(\frac{1}{50 \times 10^3} \right) \div 1 \times 10^{-3} \right] \times 100 = 2\%$$

4.26 An enhancement PMOS transistor has $k'_p(W/L) = 80 \mu\text{A/V}^2$, $V_t = -1.5 \text{ V}$, and $\lambda = -0.02 \text{ V}^{-1}$. The gate is connected to ground and the source to +5 V. Find the drain current for $v_D = +4 \text{ V}$, $+1.5 \text{ V}$, 0 V , and -5 V .



$$k'_p \times \frac{W}{L} = 80 \mu\text{A/V}^2$$

Case 1: $V_D = 4 \text{ V}$,

$$V_{SG} = 5 - 0 = 5 \text{ V} > |V_t| \Rightarrow \text{not cutoff!} \quad V_{DG} = 4 - 0 = 4 \text{ V is not } \leq |V_t| \Rightarrow \text{in Triode!}$$

$$I_D = k'_p \times \frac{W}{L} \left[(V_{SG} - |V_t|) \times V_{SD} - \frac{V_{SD}^2}{2} \right] \Rightarrow I_D = 80 \times 10^{-6} \left[(5 - |-1.5|)(5 - 4) - \frac{(5 - 4)^2}{2} \right]$$

$$I_D = 80 \times 10^{-6} \left[3.5 - \frac{1}{2} \right] = 240 \mu\text{A}$$

Case 3: $V_D = 0 \text{ V}$,

$$V_{SG} = 5 - 0 = 5 \text{ V} > |V_t| \Rightarrow \text{not cutoff!} \quad V_{DG} = 0 - 0 = 0 \text{ V} \leq |V_t| \Rightarrow \text{in Saturation!}$$

$$I_D = \frac{k'_p}{2} \times \frac{W}{L} (V_{SG} - |V_t|)^2 (1 + |\lambda| V_{SD})$$

$$I_D = \frac{80 \times 10^{-6}}{2} (5 - |-1.5|)^2 [1 + |-0.02| \times (5 - 0)] \rightarrow I_D = 40 \times 10^{-6} \times 3.5^2 \times 1.1 = 539 \mu\text{A}$$

4.44 For each of the circuits shown in Fig. P4.44, find the labeled node voltages. The NMOS transistors have $V_t = 1$ V and $k'_n W/L = 2$ mA/V². Assume $\lambda = 0$.

Assuming that the lower MOSFET is in saturation:

$$\frac{k'_n W}{2 \times L} (-V_2 - 1)^2 = \frac{V_2 - (-5)}{1} \rightarrow V_2^2 + 2V_2 + 1 = V_2 + 5$$

$$\rightarrow V_2^2 + V_2 - 4 = 0 \rightarrow V_2 = \frac{-1 \pm \sqrt{1 - [4 \times 1 \times (-4)]}}{2 \times 1} = \frac{-1 \pm \sqrt{17}}{2} = 1.56 \text{ V or } \boxed{-2.56 \text{ V}}$$

We choose -2.56 V for which $V_{GS} > V_t$ (to avoid cutoff).

$$\rightarrow I_D = \frac{k'_n W}{2 \times L} (-V_2 - 1)^2 = 1 \times 10^{-3} \times (2.56 - 1)^2 = 2.433 \text{ mA.}$$

$$\text{OR } I_D = \frac{-2.56 - (-5)}{1} = 2.44 \text{ mA (difference due to rounding!)}$$

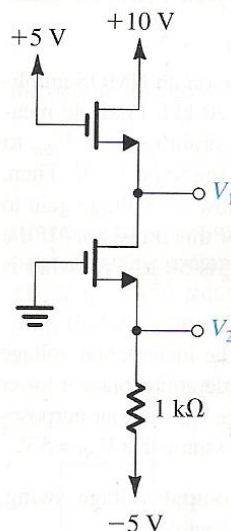
The upper MOSFET is in saturation because $V_{GD} \leq V_t$ ($-5 \leq 1$) \rightarrow

$$\frac{k'_n W}{2 \times L} (5 - V_1 - 1)^2 = 2.44 \rightarrow V_1^2 - 8V_1 + 13.56 = 0$$

$V_1 = \boxed{2.44 \text{ V}}$ or 5.562 V, we choose 2.44 V for which $V_{GS} > V_t$ (to avoid cutoff).

To verify that the lower MOSFET is in saturation:

$V_{GD} = V_G - V_D = 0 - V_1 = -2.44$ V which is indeed $\leq V_t \rightarrow$ saturated as assumed.



In the circuit shown, transistors are characterized by $|V_t| = 2 \text{ V}$, $k'W/L = 1 \text{ mA/V}^2$, and $\lambda = 0$. Find V_6 and V_7 .

Both MOSFET's are in saturation because $V_{DG} = 0 \leq |V_t|$;

Considering the upper MOSFET:

$$I_D = \frac{k'_n W}{2 \times L} (10 - V_6 - 2)^2 \rightarrow 2 = \frac{1}{2} (10 - V_6 - 2)^2 \rightarrow V_6^2 - 16V_6 + 64 = 4$$

Solving for V_6 by any method:

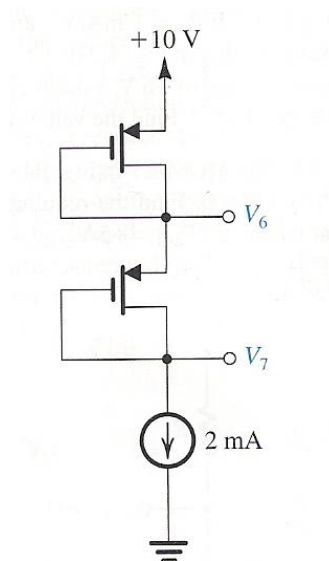
$V_6 = \boxed{6 \text{ V}}$ or 10 V, we choose 6 V for which $V_{SG} > |V_t|$ (to avoid cutoff).

For the lower MOSFET:

$$I_D = \frac{k'_n W}{2 \times L} (6 - V_7 - 2)^2 \rightarrow 2 = \frac{1}{2} (6 - V_7 - 2)^2 \rightarrow V_7^2 - 8V_7 + 16 = 4$$

Solving for V_7 by any method:

$V_7 = \boxed{2 \text{ V}}$ or 6 V, we choose 2 V for which $V_{SG} > |V_t|$ (to avoid cutoff).



4.48 In the circuit of Fig. P4.48, transistors Q_1 and Q_2 have $V_t = 1$ V, and the process transconductance parameter $k'_n = 100 \mu\text{A}/\text{V}^2$. Assuming $\lambda = 0$, find V_1 , V_2 , and V_3 for each of the following cases:

(a) $(W/L)_1 = (W/L)_2 = 20$

The $200\text{-}\mu\text{A}$ current will divide equally between Q_1 and Q_2 because their gates are at the same potential ($V_{GS1} = V_{GS2}$, $\lambda = 0$) $\rightarrow I_{D1} = I_{D2} = 100 \mu\text{A}$.

Assuming both MOSFET's are in saturation:

$$I_{D1} = \frac{k'_n W}{2 \times L} (0 - V_3 - 1)^2 \rightarrow V_3 + 1 = \pm \sqrt{\frac{100 \times 10^{-6}}{100 \times 10^{-6} \times 20}} \rightarrow V_3 = -1 \pm \sqrt{0.1} = -1.32 \text{ V or } -0.684 \text{ V}$$

Select the first value because it implies that $V_{GS} > V_t$ and thus $I_D \neq 0$ (to avoid cutoff)

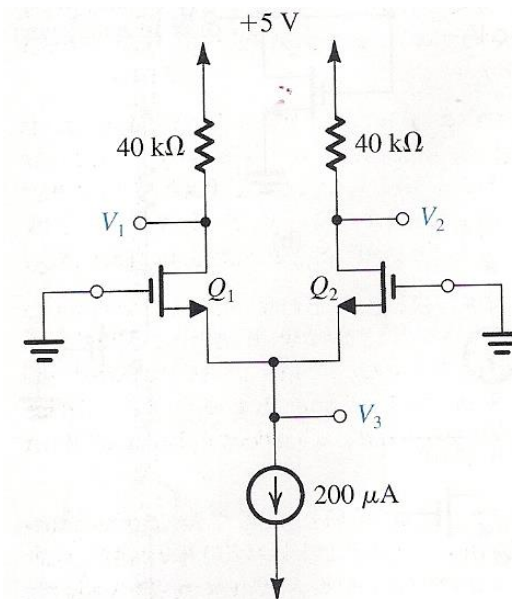
Now,

$$V_1 = V_2 = 5 - 0.1 \times 10^{-3} \times 40 \times 10^3 = 1 \text{ V}.$$

To make sure both MOSFET's are actually in saturation, we find V_{GD1} and V_{GD2} :

$$V_{GD1} = 0 - V_1 = -1 \leq V_t \rightarrow \text{saturated as assumed!}$$

$$V_{GD2} = 0 - V_2 = -1 \leq V_t \rightarrow \text{saturated as assumed!}$$

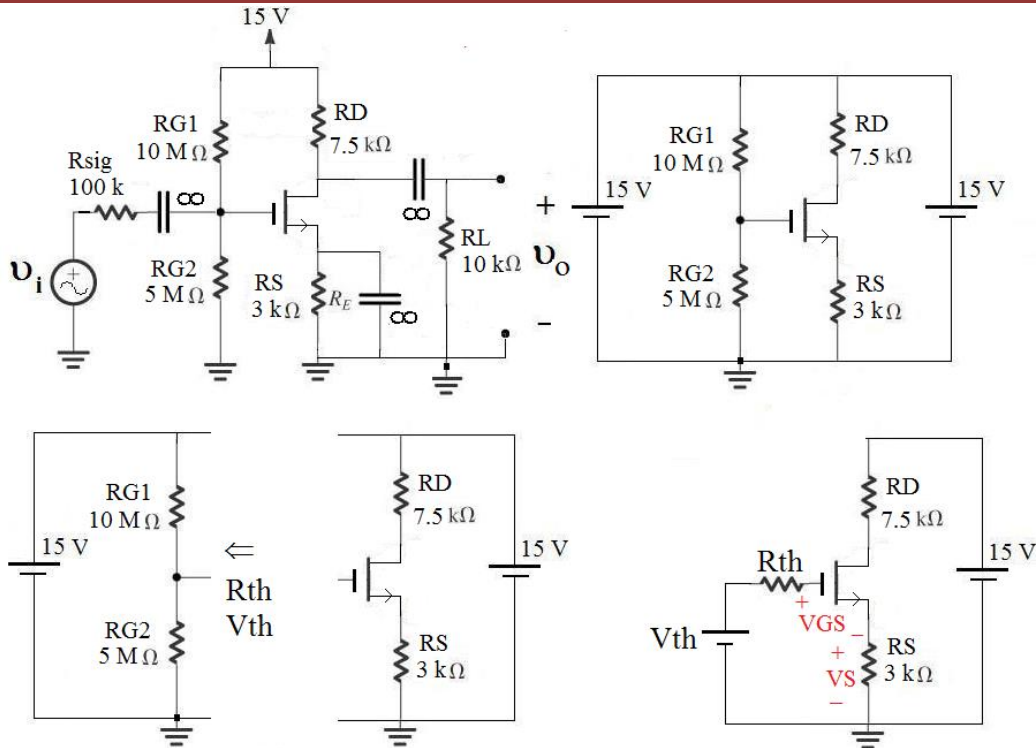


Problem 4.77, page 370, 5th ed. Sedra/Smith

a) If the transistor has $V_t = 1$ V, and $k'_n = 2$ mA/V², verify that the bias circuit establishes $V_{GS} = 2$ V, $I_D = 1$ mA and $V_D = 7.5$ V.

b) Find g_m , and r_o if $V_A = 100$ V.

c) Find R_{in} , $\frac{v_{gs}}{v_{sig}}$, $\frac{v_o}{v_{gs}}$, $\frac{v_o}{v_{sig}}$.



a)

$$R_{th} = 10 \text{ M}\Omega \parallel 5 \text{ M}\Omega = \frac{5 \times 10}{5 + 10} = 3.34 \text{ M}\Omega.$$

$$V_{th} = \left(\frac{5}{5 + 10} \right) \times 15 = 5 \text{ V}.$$

$$V_G = V_{th} \text{ (I}_G = 0\text{)}, V_{GS} = 2 \text{ (given),}$$

$$V_{GS} = V_G - V_S \Rightarrow V_S = V_G - V_{GS} = V_{th} - V_{GS} = 3 \text{ V}$$

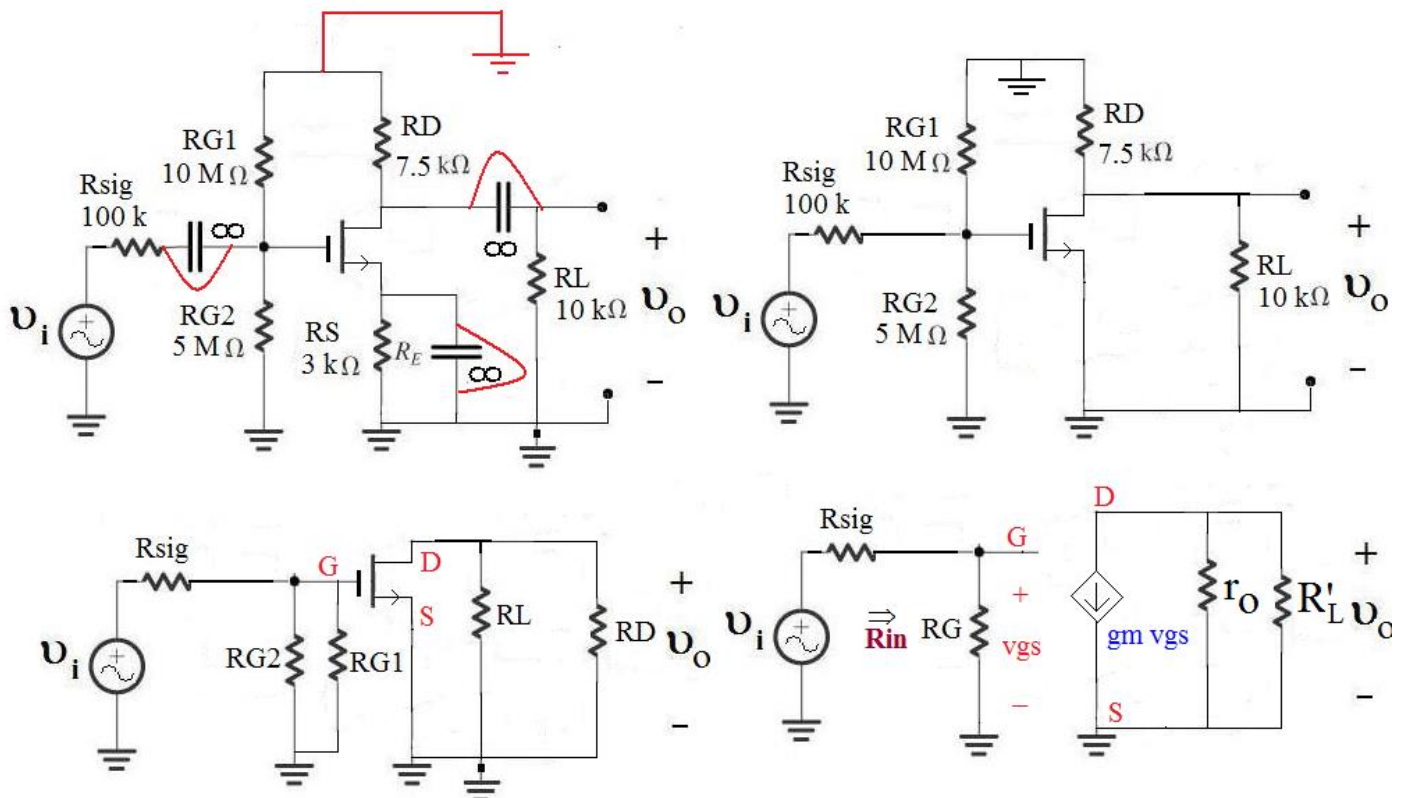
$$I_D = \frac{V_S}{R_S} = \frac{3}{3 \times 10^3} = 1 \text{ mA}$$

$$V_D = V_{DD} - I_D \times R_D = 15 - 1 \times 7.5 = 7.5 \text{ V}$$

b)

$$g_m = \frac{2I_D}{V_{GS} - V_t} = \frac{2 \times 1 \times 10^{-3}}{2 - 1} = 2 \times 10^{-3} \text{ S}$$

$$r_o = \frac{V_A}{I_D} = \frac{100}{1 \times 10^{-3}} = 100 \text{ k}\Omega$$



c)

Let's call $(R_{G1} \parallel R_{G1}) \equiv R_G = 3.34 \text{ M}\Omega$, and $(R_D \parallel R_L) \equiv R'_L = 4.29 \text{ k}\Omega$

$$R_{in} = R_{G1} \parallel R_{G1} = R_G = 3.34 \text{ M}\Omega$$

$$v_{gs} = \left(\frac{R_G}{R_G + R_{sig}} \right) \times v_{sig} \text{ (VDR)} \Rightarrow \frac{v_{gs}}{v_{sig}} = \frac{R_G}{R_G + R_{sig}} = \frac{3.34}{3.34 + 0.1} = 0.97 \text{ V/V}$$

$$v_o = -g_m \times v_{gs} \times (R'_L \parallel r_o) \Rightarrow \frac{v_o}{v_{gs}} = -g_m \times (R'_L \parallel r_o) = -2 \times 10^{-3} \times (4.29 \parallel 100) = -8.23 \text{ V/V}$$

$$\frac{v_o}{v_{sig}} = \frac{v_{gs}}{v_{sig}} \times \frac{v_o}{v_{gs}} = 0.97 \times (-8.23) = -7.98 \text{ V/V}$$
