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CHAPTER 13 GAS MIXTURES

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COMPOSITION OF A GAS MIXTURE: MASS AND MOLE FRACTIONS

To determine the properties of a mixture, we need to know the *composition* of the mixture as well as the properties of the individual components. There are two ways to describe the composition of a mixture:



FIGURE 13–1

The mass of a mixture is equal to the sum of the masses of its components.



FIGURE 13-2

The number of moles of a nonreacting mixture is equal to the sum of the number of moles of its components.

Molar analysis: specifying the number of moles of each component Gravimetric analysis:

specifying the mass of each component

$$m_{m} = \sum_{i=1}^{k} m_{i} \qquad N_{m} = \sum_{i=1}^{k} N_{i}$$
$$mf_{i} = \frac{m_{i}}{m_{m}} \qquad \text{Mass} \\ \text{fraction}$$
$$y_{i} = \frac{N_{i}}{N_{m}} \qquad \text{Mole} \\ \text{fraction}$$



The sum of the mass and mole fractions of a mixture is equal to 1.

$$\sum_{i=1}^{k} \mathbf{mf}_i = 1 \quad \text{and} \quad \sum_{i=1}^{k} y_i = 1$$

The molar mass of a mixture

$$M_{m} = \frac{m_{m}}{N_{m}} = \frac{m_{m}}{\sum m_{i}/M_{i}} = \frac{1}{\sum m_{i}/(m_{m}M_{i})} = \frac{1}{\sum_{i=1}^{k} \frac{\mathrm{mf}_{i}}{M_{i}}}$$

Mass and mole fractions of a mixture are related by

$$\mathrm{mf}_i = \frac{m_i}{m_m} = \frac{N_i M_i}{N_m M_m} = y_i \frac{M_i}{M_m}$$

$$H_{2} + O_{2}$$

$$y_{H_{2}} = 0.75$$

$$y_{O_{2}} = \frac{0.25}{1.00}$$

FIGURE 13–3

The sum of the mole fractions of a mixture is equal to 1.

P-v-T BEHAVIOR OF GAS MIXTURES: IDEAL AND REAL GASES



FIGURE 13-5

Dalton's law of additive pressures for a mixture of two ideal gases.



FIGURE 13-6

Amagat's law of additive volumes for a mixture of two ideal gases.

The prediction of the P-v-T behavior of gas mixtures is usually based on two models:

Dalton's law of additive

pressures: The pressure of a gas mixture is equal to the sum of the pressures each gas would exert if it existed alone at the mixture temperature and volume.

Amagat's law of additive

volumes: The volume of a gas mixture is equal to the sum of the volumes each gas would occupy if it existed alone at the mixture temperature and pressure. $\begin{array}{ll} Dalton's \ law: & P_m = \sum_{i=1}^{k} P_i(T_m, V_m) \\ Amagat's \ law: & V_m = \sum_{i=1}^{k} V_i(T_m, P_m) \end{array}$

exact for ideal gases, approximate for real gases

 P_i component pressure P_i/P_m pressure fraction V_i component volume V_i / V_m volume fraction

For ideal gases, Dalton's and Amagad's laws are identical and give identical results.



FIGURE 13-7

The volume a component would occupy if it existed alone at the mixture *T* and *P* is called the *component volume* (for ideal gases, it is equal to the partial volume y_iV_m).

Ideal-Gas Mixtures

$\frac{P_i(T_m,V_m)}{P_m} =$	$=\frac{N_i R_u T_m / V_m}{N_m R_u T_m / V_m} =$	$=\frac{N_i}{N_m}=y_i$
$\frac{V_i(T_m, P_m)}{V_m}$	$=\frac{N_i R_u T_m / P_m}{N_m R_u T_m / P_m} =$	$=\frac{N_i}{N_m}=y_i$

$$\blacktriangleright \frac{P_i}{P_m} = \frac{V_i}{V_m} = \frac{N_i}{N_m} = y_i$$

This equation is only valid for ideal-gas mixtures as it is derived by assuming ideal-gas behavior for the gas mixture and each of its components.

The quantity $y_i P_m$ is called the **partial pressure** (identical to the *component pressure* for ideal gases), and the quantity $y_i V_m$ is called the **partial volume** (identical to the *component volume* for ideal gases).

Note that for an ideal-gas mixture, the mole fraction, the pressure fraction, and the volume fraction of a component are identical.

The composition of an ideal-gas mixture (such as the exhaust gases leaving a combustion chamber) is frequently determined by a volumetric analysis (Orsat Analysis).

Compressibility factor

$$PV = ZNR_uT$$
 $Z_m = \sum_{i=1}^{\kappa} y_i Z_i$

 Z_i is determined either at T_m and V_m Dalton's law) or at T_m and P_m (Amagat's law) for each individual gas. Using Dalton's law gives more accurate results.



FIGURE 13-8

One way of predicting the P-v-T behavior of a real-gas mixture is to use compressibility factor.

Real-Gas Mixtures

Kay's rule

Pseudopure substance



Another way of predicting the P-v-T behavior of a real-gas mixture is to treat it as a pseudopure substance with critical properties P'_{cr} and T'_{cr} .

 Z_m is determined by using these pseudocritical properties. The result by Kay's rule is accurate to within about 10% over a wide range of temperatures and pressures.

PROPERTIES OF GAS MIXTURES: IDEAL AND REAL GASES

(kJ)

Extensive properties of a gas mixture

$$U_{m} = \sum_{i=1}^{k} U_{i} = \sum_{i=1}^{k} m_{i} u_{i} = \sum_{i=1}^{k} N_{i} \overline{u}_{i} \qquad (kJ)$$

$$H_m = \sum_{i=1}^{k} H_i = \sum_{i=1}^{k} m_i h_i = \sum_{i=1}^{k} N_i \overline{h}_i$$

$$S_m = \sum_{i=1}^k S_i = \sum_{i=1}^k m_i s_i = \sum_{i=1}^k N_i \overline{s}_i$$
 (kJ/K)

2 kmol A 6 kmol B $U_A = 1000 \text{ kJ}$ $U_B = 1800 \text{ kJ}$ $U_m = 2800 \text{ kJ}$

FIGURE 13–11

The extensive properties of a mixture are determined by simply adding the properties of the components.

Changes in properties of a gas mixture

$$\Delta U_m = \sum_{i=1}^k \Delta U_i = \sum_{i=1}^k m_i \,\Delta u_i = \sum_{i=1}^k N_i \,\Delta \overline{u}_i \qquad (kJ)$$
$$\Delta H_m = \sum_{i=1}^k \Delta H_i = \sum_{i=1}^k m_i \,\Delta h_i = \sum_{i=1}^k N_i \,\Delta \overline{h}_i \qquad (kJ)$$
$$\Delta S_m = \sum_{i=1}^k \Delta S_i = \sum_{i=1}^k m_i \,\Delta s_i = \sum_{i=1}^k N_i \,\Delta \overline{s}_i \qquad (kJ/K)$$

8

Extensive properties of a gas mixture

$$u_{m} = \sum_{i=1}^{k} \mathrm{mf}_{i} u_{i} \quad (\mathrm{kJ/kg}) \quad \text{and} \quad \overline{u}_{m} = \sum_{i=1}^{k} y_{i} \overline{u}_{i} \quad (\mathrm{kJ/kmol})$$

$$h_{m} = \sum_{i=1}^{k} \mathrm{mf}_{i} h_{i} \quad (\mathrm{kJ/kg}) \quad \text{and} \quad \overline{h}_{m} = \sum_{i=1}^{k} y_{i} \overline{h}_{i} \quad (\mathrm{kJ/kmol})$$

$$s_{m} = \sum_{i=1}^{k} \mathrm{mf}_{i} s_{i} \quad (\mathrm{kJ/kg \cdot K}) \quad \text{and} \quad \overline{s}_{m} = \sum_{i=1}^{k} y_{i} \overline{s}_{i} \quad (\mathrm{kJ/kmol \cdot K})$$

$$c_{\nu,m} = \sum_{i=1}^{k} \mathrm{mf}_{i} c_{\nu,i} \quad (\mathrm{kJ/kg \cdot K}) \quad \text{and} \quad \overline{c}_{\nu,m} = \sum_{i=1}^{k} y_{i} \overline{c}_{\nu,i} \quad (\mathrm{kJ/kmol \cdot K})$$

$$c_{p,m} = \sum_{i=1}^{k} \mathrm{mf}_{i} c_{p,i} \quad (\mathrm{kJ/kg \cdot K}) \quad \text{and} \quad \overline{c}_{p,m} = \sum_{i=1}^{k} y_{i} \overline{c}_{p,i} \quad (\mathrm{kJ/kmol \cdot K})$$

Properties per unit mass involve mass fractions (mf_i) and properties per unit mole involve mole fractions (y_i) .

The relations are exact for ideal-gas mixtures, and approximate for real-gas mixtures.

2 kmol A 3 kmol B $\overline{u}_A = 500 \text{ kJ/kmol}$ $\overline{u}_B = 600 \text{ kJ/kmol}$ $\overline{u}_m = 560 \text{ kJ/kmol}$

FIGURE 13–12

The intensive properties of a mixture are determined by weighted averaging.

Ideal-Gas Mixtures

Gibbs–Dalton law: Under the ideal-gas approximation, the properties of a gas are not influenced by the presence of other gases, and each gas component in the mixture behaves as if it exists alone at the mixture temperature T_m and mixture volume V_m .

Also, the *h*, *u*, c_v , and c_p of an ideal gas depend on temperature only and are independent of the pressure or the volume of the ideal-gas mixture.

$$\Delta s_i = s_{i,2}^{\circ} - s_{i,1}^{\circ} - R_i \ln \frac{P_{i,2}}{P_{i,1}} \cong c_{p,i} \ln \frac{T_{i,2}}{T_{i,1}} - R_i \ln \frac{P_{i,2}}{P_{i,1}}$$

$$\Delta \,\overline{s}_{i} = \,\overline{s}_{i,2}^{\circ} \, - \,\overline{s}_{i,1}^{\circ} \, - R_{u} \ln \frac{P_{i,2}}{P_{i,1}} \cong \,\overline{c}_{p,i} \ln \frac{T_{i,2}}{T_{i,1}} - R_{u} \ln \frac{P_{i,2}}{P_{i,1}}$$

 $P_{i,2} = y_{i,2}P_{m,2}$ $P_{i,1} = y_{i,1}P_{m,1}$



FIGURE 13–13

Partial pressures (not the mixture pressure) are used in the evaluation of entropy changes of ideal-gas mixtures.